

# Kinetic modelling of respiratory aerosols, numerical treatment

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involving:

C. Grandmont, B. Grec, D. Yakoubi (2D);

C. Grandmont, A. Lorz, A. Moussa (3D);

P. Diot, S. Ehrmann, L. Vecellio (experimental comparisons).

# Motivations

Studying aerosol transport in the upper part of the respiratory system  
(**aerosoltherapy**)

- Asthma, allergy, cystic fibrosis (mucoviscidosis)...
- *In vivo* observations are difficult.
- Non invasive treatments by aerosol are used for decades.
- Main issue: **locating the aerosol deposition**



This study can also be used for polluting particles in the atmosphere.

# Outline

- 1 Fluid/kinetic models for aerosols
- 2 Numerical implementation and validations
- 3 Experimental comparisons

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## Which model?

**Air:** viscous, Newtonian, incompressible fluid, described through its **density**  $\rho$ , **velocity**  $u$ , and **pressure**  $p$ , depending on  $t \geq 0$  and  $x \in \Omega$

**Aerosol:**

- Differential system on a high number of aerosol particles/droplets: most commonly used, low numerical efficiency (up to  $10^{10}$  particles)
- PDEs on **macroscopic quantities** (density, velocity...), only depending on  $t \geq 0$  and  $x \in \Omega$  [Wall *et al.*]
- PDE on a **distribution function**  $f \geq 0$  depending on  $t \geq 0$ ,  $x \in \Omega$ ,  $v \in \mathbb{R}^3$  and other variables describing the dynamical/thermodynamical/... state of the particles

## Spray models

A generical example:

$$\left\{ \begin{array}{l} \partial_t(\alpha \varrho) + \nabla_x \cdot (\alpha \varrho u) = 0 \\ \partial_t(\alpha \varrho u) + \nabla_x \cdot (\alpha \varrho u \otimes u) + \nabla_x p = \mathcal{F}_{\text{aero}} \\ \partial_t f + \nabla_x \cdot (fv) + \nabla_v \cdot (fa) + \partial_r(f\Phi) = Q(f,f) \end{array} \right.$$

- $Q(f,f)$  operator describing binary interactions between particles
- $\alpha$  fluid volume fraction
- $\mathcal{F}_{\text{aero}}$  action exerted by the particles on the fluid

For respiratory aerosol and airborne polluting particles:  $Q(f,f) \simeq 0$ ;  $\alpha \simeq 1$

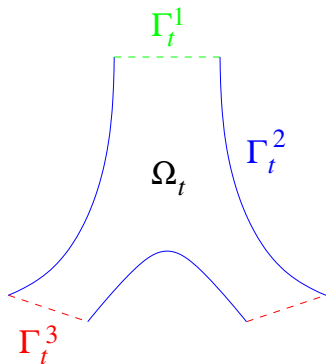
## Vlasov/(incompressible) Navier-Stokes system

$$\left\{ \begin{array}{l} \partial_t u + (u \cdot \nabla_x)u + \frac{1}{\varrho} \nabla_x p = \frac{\mu}{\varrho} \Delta_x u - \frac{1}{\varrho} \iint m a f dv dr \\ \nabla_x \cdot u = 0 \\ \partial_t f + \nabla_x \cdot (fv) + \nabla_v \cdot (fa) = 0 \end{array} \right.$$

- Particle acceleration  $a = D(u - v)$
- Drag coefficient  $D = \frac{6\pi\mu r}{m}$
- Boundary condition on  $f$ : given at the inlet

# Boundary conditions for the fluid

Geometry: possibly moving domain



- Artificial boundaries  $\Gamma_t^1$  and  $\Gamma_t^3$ :  
 $u$  imposed at the inlet, or  
 difference of pressure  
 between inlet and outlet
- Physical boundary  $\Gamma_t^2$  :  
 $u(t, x) = w(t, x)$  for  $x \in \Gamma_t^2$ ,  
 where  $w$  is the wall velocity



# Decreasing energy

## Proposition

When  $\Omega_t = \Omega_0$  for any  $t \geq 0$ ,  
 if  $u \equiv 0$  on  $\partial\Omega_0$  and if  $f \equiv 0$  on  $\partial\Omega_0 \times \mathbb{R}^3$  for  $v \cdot n_0 < 0$ , then

$$\frac{d}{dt} \left( \frac{1}{2} \iint_{\Omega_0 \times \mathbb{R}^3} f(t, x, v) m v^2 dv dx + \frac{1}{2} \int_{\Omega_0} \rho u(t, x)^2 dx \right) \leq 0.$$

⇒ this property should also be satisfied at the discrete level.

**Existence result:** LB, L. Desvillettes, C. Grandmont, A. Moussa, DIE '09  
 see also Anochschenko, Boutet de Monvel '97; Hamdache '98; Yu '13

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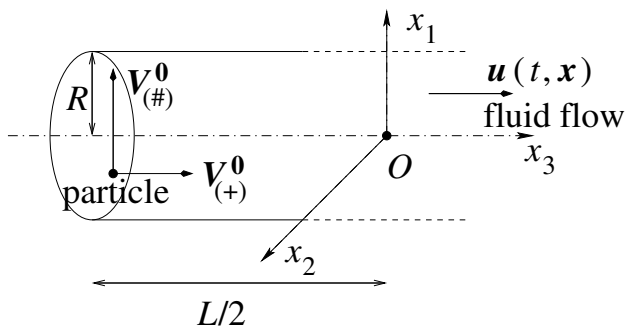
# Discretization (w/ C. Grandmont, A. Moussa)

- Explicit time-advancing scheme  $\implies$  uncoupling the equations
  - ① Solving the Navier-Stokes equations with the retroaction term coming from the previous time step
  - ② Solving the Vlasov equation by using the fluid velocity updated at the previous stage
  - ③ Computing the new retroaction term to be used at the next time step (possibly with a time subcycling)
- Space discretization
  - ▶ Fluid: finite element method with an ALE approach (moving domain)
  - ▶ Aerosol: particle method with a locating algorithm

$$f(t, x, v) \simeq \sum_{p=1}^N \omega_p \delta_{x_p(t)}(x) \delta_{v_p(t)}(v)$$

$N \ll \#$  phys. particles;  $\omega_p$  representativity of particle  $p$

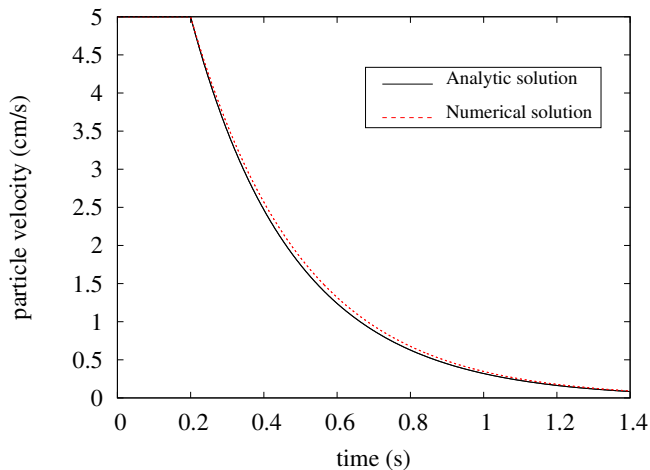
## Validation frame (w/ CG, A. Lorz and AM)



- Fluid:  $u(t, x) = U \times \left( 1 - \frac{x_1^2 + x_2^2}{R^2} \right)$
- Particles: same size, density and initial velocity  $V^0$

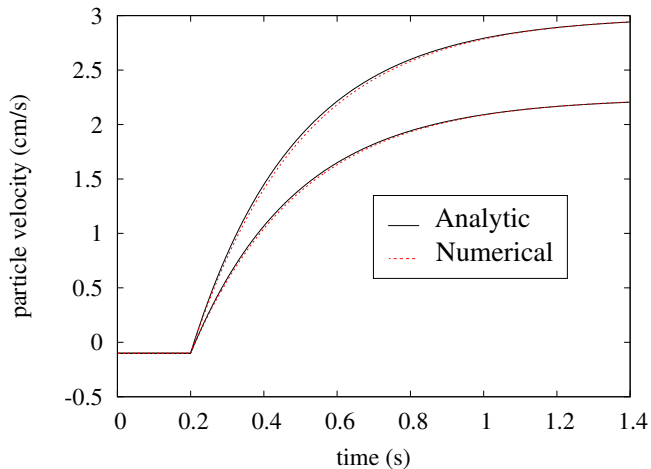
# Motionless fluid in a fixed domain, w/o retroaction

One can find an analytic solution to the particles trajectories.



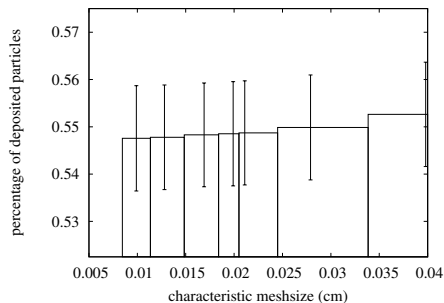
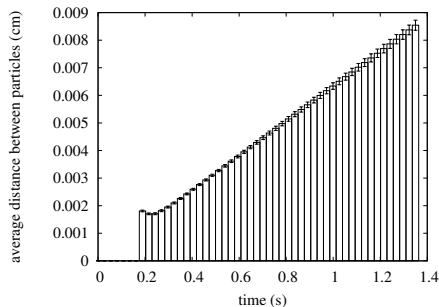
## Moving fluid in a fixed domain, w/o retroaction

One can also find an analytic solution to the particles trajectories.



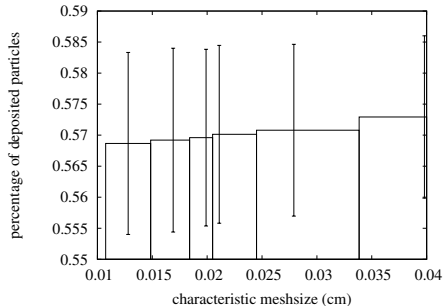
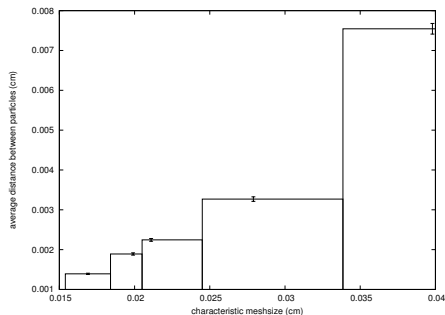
# Sensitivities

Various test-cases with varying meshes, time steps, initial data on  $f$



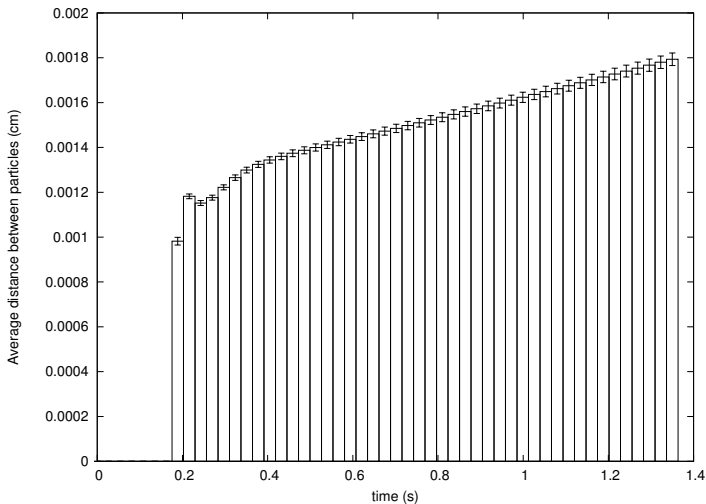
## Sensitivities in a moving domain, w/o retroaction

Validation of the fluid code in a 2D moving domain thanks to an analytic solution computed in cylindrical coordinates



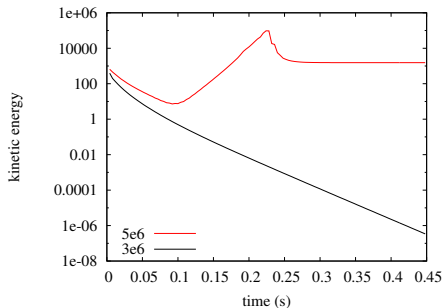
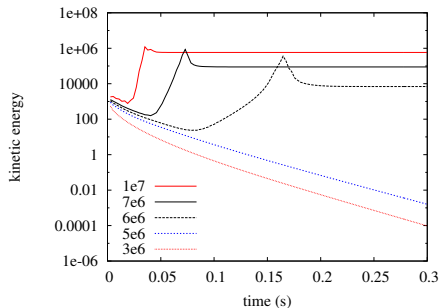


## Sensitivities in a fixed domain, w/ retroaction



# Representativities (1)

$N$  constant (numerical particles)

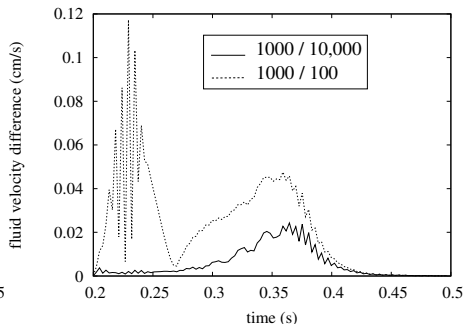
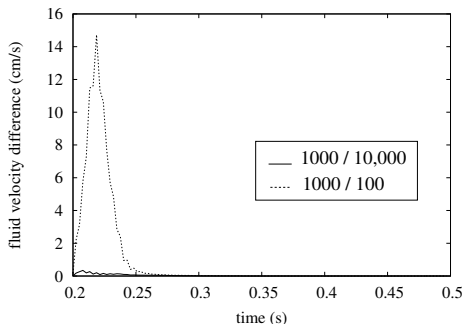


⇒ existence of a CFL-like condition involving, amongst others,  $\omega_p \Delta t$

$$\text{cf. } \mathcal{F}_{\text{aero}}^n(x) = -m \sum_{p=1}^N \omega_p D \left( \tilde{u}^n(x_p^n) - v_p^n \right) \delta_{x_p^n}(x) \text{ for } x \in \Omega_{t^n}$$

## Representativities (2)

$N\omega_p$  constant (physical particles)



Study assessment:

for particles with radius  $\leq 25 \mu\text{m}$ , retroaction can be neglected.

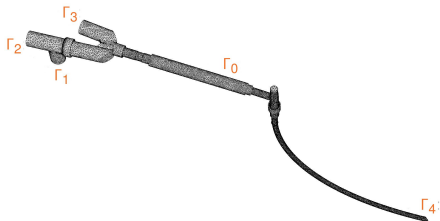
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# Joint work with Aerodrug/DTF

Goal: compare experimental and numerical results

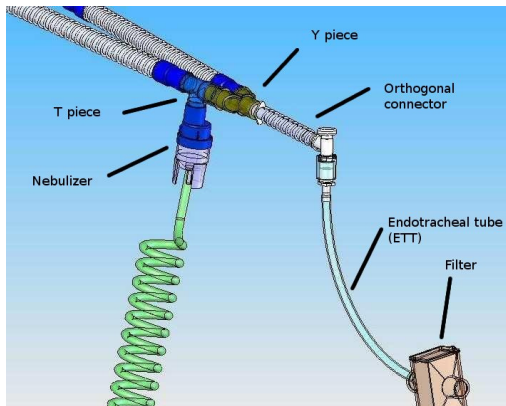
Retroaction neglected



- Need an accurate location of the aerosol deposition areas
- *In vitro*: 3D imaging by scintigraphy, Gamma camera
- *In silico*: LifeV, finite element fluid solver in C++, with actual development of the particle solver

# Simulation on an endotracheal tube

Filter collecting aerosol at the ETT outlet



# Simulation on an endotracheal tube

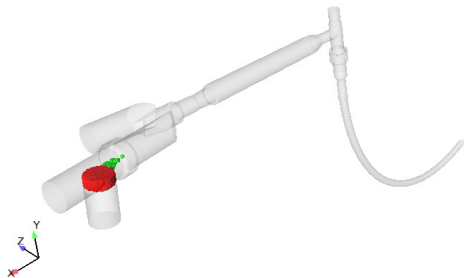
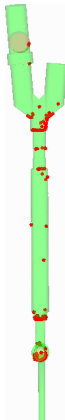
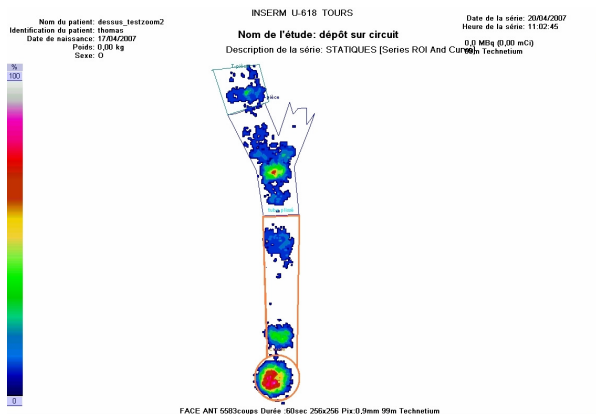


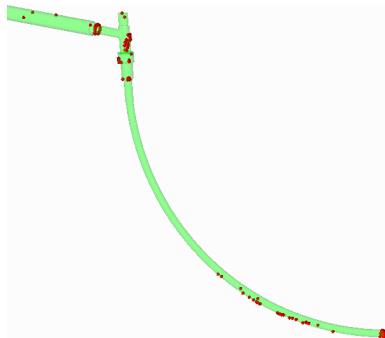
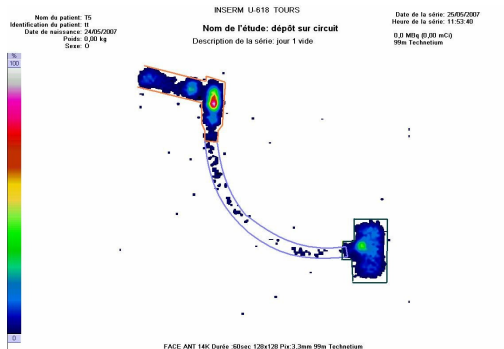
Figure: Device mesh designed by M. Grasseau. 

## Deposition areas, view from above





# Deposition areas, lateral view



# Deposition rate

## Experimental results

VMD/flow rate	10 L/min	20 L/min	40 L/min
5.4 $\mu\text{m}$	29%	41%	60%
14 $\mu\text{m}$	42%	73%	86%

## Numerical results

(averaged on 10 random distributions of particles)

diam./flow rate	10 L/min	20 L/min	40 L/min
5.4 $\mu\text{m}$	32%	45%	72%
14 $\mu\text{m}$	41%	76%	98%

# Prospects and ongoing works

- Mathematical analysis (w/ C. Grandmont and A. Moussa):  
existence of solutions in a moving domain
- Validation by experimental comparisons in a moving domain (in a pluridisciplinary ANR-supported team and headed by M. Filoche)
- Engeneering on aerosol nebulizers in a fixed domain (w/ Aerodrug)
- Nanometric aerosols modelling, humidity effect (w/ C. Rigault)